



3rd Conference on Sustainability in Civil Engineering (CSCE'21)
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Capital University of Science and Technology, Islamabad Pakistan

PREDICTING THE IMPACT OF CHEMICAL AND PHYSICAL VARIABILITY IN BINARY AND TERNARY CEMENTITIOUS BLENDS

^a Vireen Limbachiya, ^b Rabee Shamass,*

a: Civil and Building Services Engineering, London South Bank University, limbachv@lsbu.ac.uk

b: Civil and Building Services Engineering, London South Bank University, shamassr@lsbu.ac.uk

* Corresponding author: Email ID: limbachv@lsbu.ac.uk

Abstract- To reduce the quantity of CO₂ emitted within the construction industry, cementitious by-products will need to be implemented on a larger scale. In relation to the use of by-products, one of the biggest disadvantages is that not only from source to source, obtaining a by-product from the same source could result in a variation in the chemical and physical properties which will then impact the mechanical properties. Therefore, the paper reviewed binary and ternary cementitious pastes that were produced from 7 different by-products and predicted the impact of variation in the chemical and physical properties on the 14-day compressive strength. The predictions and analysis were done with the use of artificial neural networks (ANN). Overall, ANN successfully derived an accurate prediction which correlated with the trends that were expected. This study noted that if parameters of the overall mix were taken into consideration, the increase in SiO₂ will have a negative impact while increase in CaO would have a positive impact on the 14-day strength. The most accurate form of understanding the impact of chemical and physical variability of cementitious replacements, took into consideration both Ca/Si ratio and the average particle size.

Keywords- ANN, Cement Replacements, Predicting Compressive Strength, Binary and Ternary Cementitious Pastes.

1 Introduction

Studies have reviewed many combinations of cementitious by-products that can be used as an alternative for Ordinary Portland Cement (OPC) [1,2]. The impact of Pulverised Fuel Ash (PFA) and By-Pass Dust (BPD) obtained over a 6-month period from the same source was analysed by Limbachiya et al [3]. The results showed a clear variation in the chemical and physical properties and the correlating impact on strength development. Shi et al. [4] reported on four different forms of glass powder being used as a cementitious replacement. They noted that the particle size has a large effect on the compressive strength of concrete, as replacements containing larger particles size produced lower strengths at 28 days. Overall results showed one of the biggest disadvantages of using by-products is that not only from source to source, obtaining a by-product from the same source could result in a variation in the chemical and physical properties, which thereafter will result in a variation in concrete strength.

When there is variation in OPC, Bogues equations are used to predict the quantity of compounds that will be produced during the hydration process and therefore, an indication of strength development. Bogues equations use the oxide composition of OPC to determine the level of alite, belite, tricalcium aluminate and tetracalcium aluminoferrite [5], which are responsible for different properties within concrete. As well as the individual oxide values, oxide ratios are known to help predict the behaviour of concrete. In a review of the influence of the Ca/Si ratio on the compressive strength of cementitious calcium–silicate–hydrate binders, it was concluded that as Ca/Si ratio decreases the compressive strength increase [6]. It was reported that the diffraction peaks' intensity of calcite became stronger as the Al/Si ratio decreases [7]. It is assumed that as the Al/Si ratio increases the calcite decreases, therefore, greater formation of strength gaining compounds. Finally, it was concluded that for lower ratios of Mg/Si, unreacted silica remained and for higher ratios brucite precipitated. Therefore, greater forms of deterioration are likely to occur at higher ratio levels [8].



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When it comes to a variation of properties in cement replacements, there are no such tools that can be used to help understand the impact on strength development. Studies have used artificial neural networks (ANN) to predict the strength of concrete using more sustainable materials. ANN was used to understand the effect of Nano and Micro Silica on the compressive and flexural strength of cement mortar [9]. The variables in this case were the quantity of different components used in the mortar mixture. The study concluded that the ANN model was able to predict the compressive strength to a high level of accuracy. Alongside ANN, Fuzzy Logic (FL) models have been used by previous studies to help predict the behaviour of concrete [10,11]. Although both models can provide high levels of accuracy, both studies concluded that ANN provided a greater level of statistical accuracy in comparison to FL. Currently, there are very few studies that have looked at a range of chemical and physical variations in by-product combinations and the impact of this on the strength of cementitious mixes consisting of binary and ternary blends. Therefore, the aim of this study is to use ANN to predict the impact of chemical and physical variability in cementitious by-products. The objectives are to firstly, produce ternary and binary cementitious pastes. Secondly, use the chemical and physical properties of these mixes as input parameters to help predict and determine the parameters that have an impact on the compressive strength. The significance of this work is that it will allow for a better understanding on the impact of chemical and physical variability when using binary and ternary cementitious pastes and determine how ANN can be used to help predict this behaviour.

2 Research Methodology

2.1 Cementitious materials

The OPC fulfilled the requirements of BS EN 197-1 CEM I [12]. The cementitious materials used in this study were obtained from a variety of sources. Ground Granulated Blast Furnace Slag (GGBS), (PFA), Metakaolin (MK), BPD and Silica Fume (SF) came in powder form to be used within the cementitious binders, while Basic Oxygen Slag (BOS) and Glass Powder (GP) came in a crushed form and required further grinding before adequate levels of fineness were achieved. Table 1 provides the physical and chemical properties using of Hydro 2000/Mastersizer 2000 and X-Ray Fluorescence (XRF) respectively.

Table 1 Chemical and physical properties of OPC and Cement Replacements.

| Composition | SiO ₂ (%) | TiO ₂ (%) | Al ₂ O ₃ (%) | Fe ₂ O ₃ (%) | MnO (%) | MgO (%) | CaO (%) | Na ₂ O (%) | K ₂ O (%) | P ₂ O ₅ (%) | SO ₃ (%) | Average Particle Size (µm) |
|-------------|-------------------------|-------------------------|---------------------------------------|---------------------------------------|---------------|---------------|----------------|--------------------------|-------------------------|--------------------------------------|------------------------|----------------------------------|
| OPC | 19.42 | 0.36 | 4.55 | 2.49 | 0.02 | 1.03 | 60.60 | 0.22 | 0.57 | 0.2 | 3.62 | 38 |
| PFA | 45.85- 52.29 | 0.98- 0.82 | 24.43- 19.76 | 10.38- 7.55 | 0.16- 0.06 | 2.09- 1.44 | 6.13- 2.81 | 0.91- 0.63 | 2.75- 2.02 | 0.51- 0.22 | 0.84- 0.48 | 55-32 |
| GGBS | 33.28 | 0.57 | 13.12 | 0.32 | 0.32 | 7.74 | 37.16 | 0.33 | 0.48 | 0.01 | 2.21 | 20 |
| SF | 94.21 | 0.01 | 0.48 | 0.71 | 0.01 | 0.55 | 0.37 | 0.35 | 1.15 | 0.04 | 0.17 | 0.7 |
| BOS | 13.94 | 0.7 | 2.98 | 25.99 | 3.17 | 6.56 | 39.57 | 0.06 | 0.03 | 1.51 | 0.28 | 30 |
| GP | 69.56 | 0.07 | 2.01 | 0.65 | 0.32 | 1.19 | 10.61 | 12.28 | 0.98 | 0.03 | 0.18 | 100 |
| MK | 54.06 | 0.02 | 40.65 | 0.77 | 0.01 | 0.23 | 0.03 | 0.17 | 1.89 | 0.16 | 0.02 | 7 |
| BPD | 17.34- 12.79 | 0.23- 0.19 | 4.26- 3.47 | 2.36- 1.88 | 0.05- 0.04 | 1.11- 0.82 | 53.6- 44.03 | 1.16- 0.5 | 10.06- 4.28 | 0.25- 0.12 | 12.22- 6.25 | 67-32 |

2.1 Mix Design and Fabrication

130 cementitious pastes were produced, tested, and analysed by the author in the laboratory for this study. All cementitious pastes were produced as a semi dry mix with constant w/c ratio of 0.2, therefore the variability in the results could only be due to the difference in the chemical and physical properties of the materials used. To produce samples, the binary//ternary



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mixtures were mixed thoroughly before water was added and compaction was applied. Thereafter, the samples were cured and tested following guidance in BS EN1338:2003. The paste cubes had a dimension of 50x50x50mm, and the compressive strength was obtained at 14 days. The mixes produced had varying levels of OPC and by products. OPC, PFA, BPD, GGBS, GP, SF, BOS and MK was used to produce the cement pastes by up to 60%, 80%, 10%, 80%, 15%, 15%, 45% and 30% by weight respectively. All mixes can be found in Appendix A.

3. Artificial Neural Network setup

3.1 Input and target parameters

Input properties were based on the combined oxide properties of ternary and binary mixes, which were obtained by using Equation 1 that was developed for this study. Table 2 provides the actual oxide compositions determined using XRF for 11 ternary and binary mixes, as well as the predicted oxide compositions using Equation 1. Based on these results, Equation 1 was determined to provide an accurate assumption on the combined oxide percentage and therefore be used in the ANN models.

$$\text{Input}_n = \left(\frac{\% \text{OPC}}{100} * \text{OPC}_n\right) + \left(\frac{\% \text{CR1}}{100} * \text{CR1}_n\right) + \left(\frac{\% \text{CR2}}{100} * \text{CR2}_n\right) \quad (\text{Equation 1})$$

Where Input_n is the input parameter for the ANN model, %OPC is the percentage of OPC used in the mix, n represents the chemical or physical property, OPC_n is the quantity of n in OPC, %CR1 and %CR2 are the percentages of cement replacements used in the mix and CR1_n and CR2_n are the quantity of n in the cement replacement.

Table 2 Accuracy of Predicted Ternary and Binary oxides

| Mix | SiO ₂ (%) | | CaO (%) | | Al ₂ O ₃ (%) | | Fe ₂ O ₃ (%) | |
|-----|----------------------|-----------|---------|-----------|------------------------------------|-----------|------------------------------------|-----------|
| | Actual | Predicted | Actual | Predicted | Actual | Predicted | Actual | Predicted |
| 1 | 24.53 | 24.96 | 50.49 | 51.22 | 6.73 | 7.98 | 1.69 | 1.62 |
| 2 | 31.25 | 32.22 | 45.57 | 45.91 | 5.16 | 5.76 | 1.74 | 1.69 |
| 3 | 20.62 | 21.10 | 50.27 | 51.71 | 5.33 | 5.95 | 6.31 | 6.76 |
| 4 | 23.42 | 24.14 | 50.96 | 52.05 | 6.40 | 7.53 | 1.77 | 1.72 |
| 5 | 23.96 | 24.71 | 49.23 | 50.52 | 6.69 | 7.94 | 1.64 | 1.61 |
| 6 | 16.51 | 17.23 | 51.21 | 52.19 | 3.64 | 3.92 | 11.18 | 11.89 |
| 7 | 27.98 | 30.75 | 38.42 | 37.66 | 10.19 | 12.38 | 4.65 | 5.58 |
| 8 | 35.49 | 37.72 | 37.62 | 37.23 | 7.55 | 8.83 | 3.60 | 4.16 |
| 9 | 33.91 | 34.10 | 44.82 | 45.71 | 5.76 | 6.08 | 1.56 | 1.68 |
| 10 | 31.60 | 31.06 | 46.25 | 47.55 | 5.72 | 6.71 | 1.63 | 1.66 |
| 11 | 28.94 | 29.53 | 48.75 | 48.46 | 5.94 | 7.03 | 1.70 | 1.65 |

3.2 Neural Network setup.

Figures 1 and 2 show the ANN models developed in this study, namely NN 5-7 and NN 4-7. Seven neurons in the hidden layer were chosen as they provided accurate predictions. The five input parameters for NN 5-7 were based on the combined chemical properties that form alite, belite, tricalcium aluminate and tetracalcium aluminoferrite, as well as the average particle size. The four input parameters for NN 4-7 were ratios that are known to have a direct impact on hydration compounds and formation of calcium silicate hydrate (CSH) as well as the average particle size.

To have a more effective ANN setup, the input and target parameters are normalised [13]. The calculated output will then also provide a normalised value, which will require it to be reverse transformed to obtain the actual target value. To normalize the input and output parameters, Equation 2 was applied to all values. Where a_{\min} and a_{\max} are constants, b_{\max} is the greatest value of that parameter, b_{\min} is the lowest value of that parameter, b is the actual value and a is the normalised value. Table 3 provides the values required to de-normalise the values.

$$a = (a_{\max} - a_{\min}) * (b - b_{\min}) / (b_{\max} - b_{\min}) + a_{\min} \quad (\text{Equation 2})$$



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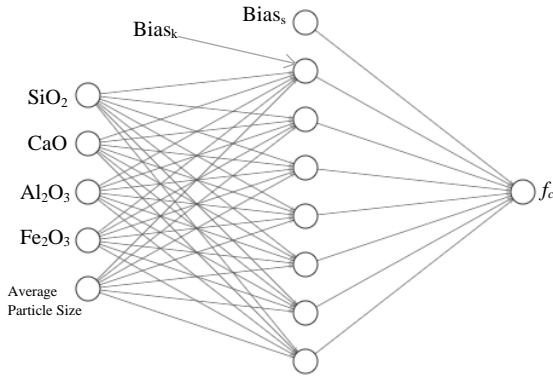


Figure 1 NN 5-7 Model

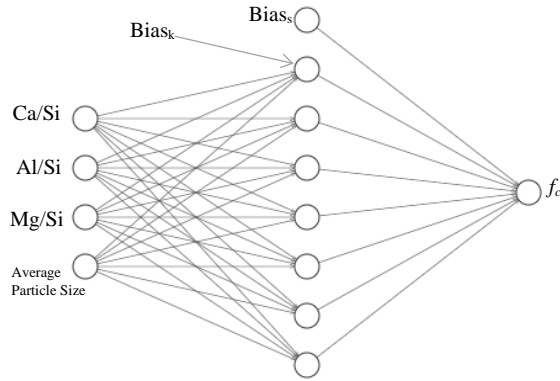


Figure 2 NN 4-7 Model.

Table 3 Parameters used to normalise input and target values

| Input/Target Parameter | a _{max} | a _{min} | b _{min} | b _{max} |
|--------------------------------|------------------|------------------|------------------|------------------|
| SiO ₂ | 1 | -1 | 16.12 | 53.30 |
| CaO | 1 | -1 | 5.69 | 60.23 |
| Al ₂ O ₃ | 1 | -1 | 3.61 | 26.34 |
| Fe ₂ O ₃ | 1 | -1 | 0.49 | 16.59 |
| Ca/Si | 1 | -1 | 0.11 | 3.15 |
| Al/Si | 1 | -1 | 0.18 | 0.58 |
| Mg/Si | 1 | -1 | 0.02 | 0.28 |
| Average Particle Size (µm) | 1 | -1 | 18.01 | 58.9 |
| f _c (MPa) | 1 | -1 | 0 | 70.40 |

Once the input and output parameters were determined, the next step was to define the neural network. A pre-installed neural network fitting app in Matlab was used in this study. The neural network fitting app solves an input-output fitting problem with a two-layer feedforward neural network. The network was a two-layer feed-forward network with sigmoid hidden neurons and linear output neurons and trained with Levenberg-Marquardt backpropagation algorithm, unless there is not enough memory, in which case scaled conjugate gradient backpropagation will be used [13]. The backpropagation algorithm involves two phases. Firstly, the forward phase where the activations are propagated from the input to the output layer [11]. Secondly, the backward phase where the error between the observed actual value and the desired nominal value in the output layer is propagated backwards to modify the weights and bias values [11]. Equations 3 and 4 provide the calculations that includes the transfer function required to determine the normalised target value based on the inputs provided [14]. Where, O_s is the normalised output value, q is the number of input parameters; r is the number of hidden neurons; s is the number of output parameters; $Bias_s$ and $Bias_k$ are the biases of s^{th} output neuron and k^{th} hidden neuron (H_k), respectively; with $w_{j,k}$ are the weights of the connection between I_j and H_k and $w_{k,l}$ are the weights of the connection between H_k and O_s .

$$O_s = Bias_s + \sum_{k=1}^r w_{k,l}^{ho} \cdot \frac{2}{(1 + e^{(-2 \times H_k)}) - 1} \quad (\text{Equation 3})$$

$$H_k = Bias_k + \sum_{j=1}^q w_{j,k}^{ih} \cdot I_j \quad (\text{Equation 4})$$

For training, validation and testing the data sets were divided into 70%, 15% and 15% respectively. To assess the accuracy of the output the regression (R^2), Root Mean Square Error (RMSE), Mean Absolute Percentage Error (MAPE) and Mean Square Error (MSE) were calculated using equations 5, 6, 7 and 8 respectively.



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$$R^2 = 1 - \left(\frac{\sum_{i=1}^N (t_i - O_i)^2}{\sum_{i=1}^N (t_i - t_m)^2} \right) \quad (\text{Equation 5})$$

$$RMSE = \sqrt{\frac{\sum_{i=1}^N (O_i - t_i)^2}{N}} \quad (\text{Equation 6})$$

$$MAPE = \frac{1}{N} \sum_{i=1}^N \left| \frac{O_i - t_i}{t_i} \right| \times 100 \quad (\text{Equation 7})$$

$$MSE = \frac{\sum_{i=1}^N (O_i - t_i)^2}{N} \quad (\text{Equation 8})$$

Where t_i is the actual compressive strength of concrete mixes, t_m is the mean compressive strength of concrete mixes, O_i is the predicted value and N is the total number of data points in each set of data.

3.3 Impact of Individual Input

As well as assessing the accuracy of the models with Equations 5 and 6, it is also important to understand the impact of input parameters on the output value. This will allow for further validation of the ANN model and algorithms, as it will have the potential to be used for values outside of those used in this model. It is important to note that the values will still have to remain within the ranges stated in Table 3. To determine the impact of each input parameter, the connection weight approach was adopted. The connection weight approach uses raw connection weights, which accounts for the direction of the input–hidden–output relationship and results in the correct identification of variable contribution [15]. Based on this approach, Equation 9 was used to determine impact of each input parameter. A negative value will mean that an increase in this parameter will decrease the output value, a positive value will mean that an increase in this parameter will increase the output value and those values with the largest value are those with the largest impact.

$$Input_x = \sum_{Y=A}^E Hidden_{XY} \quad (\text{Equation 9})$$

3 Results

3.1 Predicting the impact of chemical and physical variability

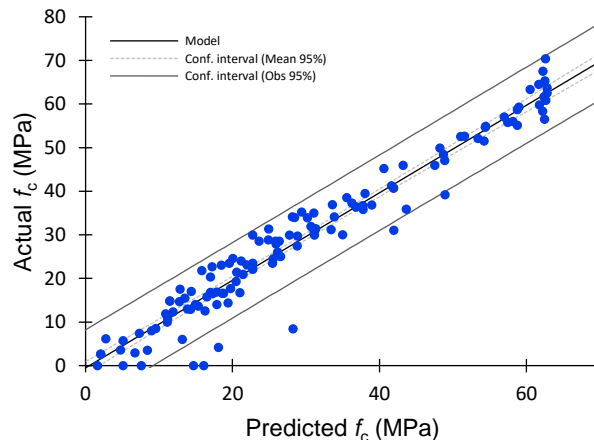


Figure 3 Regression of Actual f_c vs predicted f_c for NN 5-7

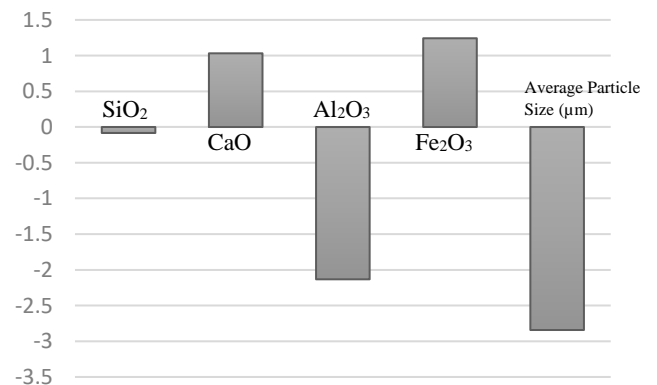


Figure 4 Influence of each input for NN 5-7



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$$f_c = -0.84 - 1.47 \left(\frac{2}{(1 + e^{(-2H_1)})} - 1 \right) - 0.29 \left(\frac{2}{(1 + e^{(-2H_2)})} - 1 \right) - 0.74 \left(\frac{2}{(1 + e^{(-2H_3)})} - 1 \right) + 1.86 \left(\frac{2}{(1 + e^{(-2H_4)})} - 1 \right) - 1.89 \left(\frac{2}{(1 + e^{(-2H_5)})} - 1 \right) - 0.25 \left(\frac{2}{(1 + e^{(-2H_6)})} - 1 \right) + 0.55 \left(\frac{2}{(1 + e^{(-2H_7)})} - 1 \right)$$

(Equation 10)

Where:

- H₁= -1.80 + 0.29SiO₂ + 0.20CaO + 1.90 Al₂O₃- 4.06Fe₂O₃ + 1.49 Average Particle Size (μm)
- H₂= 1.97 + 0.52SiO₂ - 1.01CaO + 2.29Al₂O₃ + 0.15Fe₂O₃ -0.63 Average Particle Size (μm)
- H₃= -0.03 + 1.22SiO₂ - 0.71CaO - 2.74Al₂O₃ + 0.22Fe₂O₃ - 1.19 Average Particle Size (μm)
- H₄= -0.87 + 0.25SiO₂ + 0.43CaO + 1.68Al₂O₃ - 2.27Fe₂O₃ + 0.35 Average Particle Size (μm)
- H₅= 1.08 - 0.42SiO₂ + 0.23CaO + 1.96Al₂O₃ - 0.38Fe₂O₃ - 0.42 Average Particle Size (μm)
- H₆= 1.84 + 2.71SiO₂ - 4.00CaO + 0.46Al₂O₃ - 1.37Fe₂O₃+ 3.03 Average Particle Size (μm)
- H₇= -2.42 + 1.47SiO₂ - 1.56CaO - 0.07Al₂O₃ - 2.45Fe₂O₃ - 4.36 Average Particle Size (μm)

Figure 3 provides the predicted vs experimental strengths for the NN 5-7 model. Equation 10 is derived from algorithms used in the ANN model for predicting the 14-day compressive strength. The R², RMSE, MSE and MAPE values were 0.95,4.36, 18.98 and 17.97, respectively. Overall, the results show that ANN can predict compressive strength to a high level of accuracy when oxide values are considered using Equation 1. It is assumed that the accuracy is closely related to the input parameters behaving in the way that is expected. Figure 4 provides the impact that each input parameter has on the output value. Results show that as SiO₂, Al₂O₃ and Average particle size increases, there will be a negative impact on the output and that as CaO and Fe₂O₃ increases, there is a positive impact on the output. Studies [16][17][18] have previously noted that cement replacements with a high SiO₂ content provide greater strength development through secondary reaction with Ca (OH)₂. However, when SiO₂ is determined using Equation 1, results show that overall, as SiO₂ increases the strengths tend to decrease and that as CaO increases there is an increase in strength. This therefore correlates with result that you would expect to occur in OPC hydration in which the ratio of Ca/Si dictates the formation of compounds and therefore strength development. Fe₂O₃ is the input that is responsible for the greatest strength gain. Although studies [19] have reported on the positive impact of Nano Fe₂O₃ on the compressive strength of concrete, the strength development in concrete is primarily down to the formation of Calcium silicate (Ca₃SiO₅) and Larnite (Ca₂SiO₄). Overall, the biggest impact on strength development was the average particle size. Results show that as average particle size increases the strength decreases. This correlated with conclusions made in previous studies [4] and is assumed to be due to the water not being able to react with the oxides within the inner particle of the material.

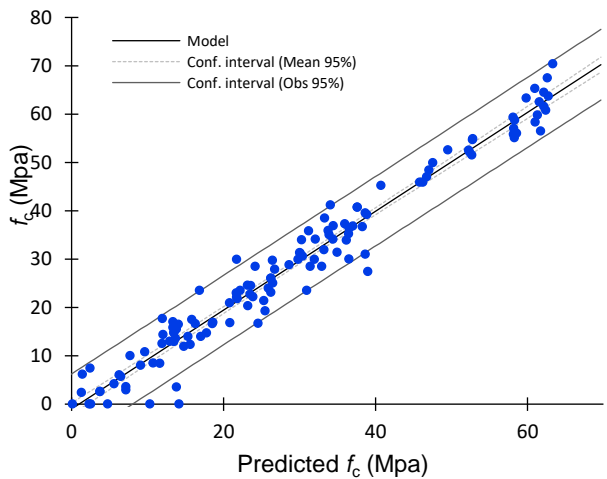


Figure 5 Regression of Actual f_c (MPa) vs predicted f_c (MPa) for NN 4-7

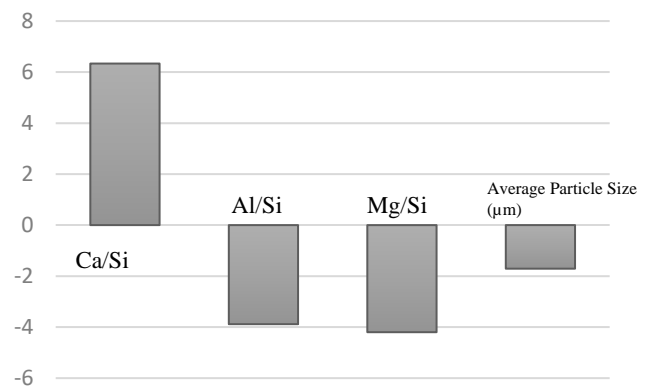


Figure 6 Influence of each input for NN 5-7-1



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$$f_c = 1.04 + 0.67 \left(\frac{2}{(1 + e^{(-2H_1)})} - 1 \right) + 0.38 \left(\frac{2}{(1 + e^{(-2H_2)})} - 1 \right) - 0.36 \left(\frac{2}{(1 + e^{(-2H_3)})} - 1 \right) + 0.64 \left(\frac{2}{(1 + e^{(-2H_4)})} - 1 \right) + 0.73 \left(\frac{2}{(1 + e^{(-2H_5)})} - 1 \right) + 1.72 \left(\frac{2}{(1 + e^{(-2H_6)})} - 1 \right) + 1.00 \left(\frac{2}{(1 + e^{(-2H_7)})} - 1 \right)$$

(Equation 11)

Where:

H₁= 1.79 + 0.34Ca/Si – 1.79Al/Si - 1.86 Mg/Si – 0.29 Average Particle Size (µm)

H₂= 1.20 – 0.43Ca/Si – 2.36Al/Si – 0.26 Mg/Si – 0.15 Average Particle Size (µm)

H₃= 0.31 – 0.66Ca/Si + 2.31Al/Si + 2.17 Mg/Si + 3.15 Average Particle Size (µm)

H₄= 0.02 – 1.16a/Si + 0.12Al/Si + 1.10 Mg/Si + 1.41 Average Particle Size (µm)

H₅= -0.74 + 0.89Ca/Si + 1.92Al/Si + 0.37 Mg/Si – 0.64 Average Particle Size (µm)

H₆= 1.76 + 2.61Ca/Si + 0.08Al/Si - 1.77 Mg/Si – 0.18 Average Particle Size (µm)

H₇= 3.96 – 1.50Ca/Si – 1.67Al/Si + 1.43 Mg/Si + 0.26 Average Particle Size (µm)

Figure 5 provides the predicted vs experimental strengths for the NN 4-7 model. Equation 11 is derived from algorithms used in the ANN model for predicting the 14-day compressive strengths. The R², RMSE, MSE and MAPE values are 0.96, 3.61, 13.05 and 14.92, respectively. In comparison to oxide percentages, oxide ratios predict output with a higher level of accuracy and a greater level of confidence. It is assumed R², RMSE, MSE and MAPE provide a greater level of accuracy as the ratios correlate to the formation of compounds that are responsible for strength development. Therefore, ANN can correlate more accurately with the output parameter. Figure 6 shows that the only ratio that contributes to strength development is Ca/Si, while Al/Si, Mg/Si and average particle size all have a negative impact. Overall, these results show that when taking into consideration the combined oxide values, the trends follow those that are noted for OPC hydration. Alite has a Ca/Si ratio of 3:1 and C-S-H has a Ca/Si ratio of approximately 2:1, so excess lime is available to produce Ca(OH)₂ [20]. Alite is responsible for early age strength development as well as formation of Ca(OH)₂ and results show that as Ca/Si increases, the trend is that strength properties will also increase. When reviewing Al/Si, trends show a decrease in strength as the ratio increases. This correlates with the results that were obtained, in which it was concluded that depending on the Al₂O₃/SiO₂ ratio, the ye'elimite and gehlenite phases were formed in different proportions [21]. It is therefore assumed that in the mixes reviewed, at lower ratios of Al/Si, content of gehlenite exceeds the ye'elimite content therefore decreasing strength properties.

4 Conclusion

The overall aim of this study was to produce an ANN system that can be used to predict the compressive strength of cement paste at 14 days and to help in gaining a better understanding of the chemical and physical properties of by-products that impact strength. Based on the report the following conclusions can be made:

- Cementitious replacements for OPC come from a variety of sources with varying chemical and physical properties. Based on the level of replacement, the use of these materials will have an impact on the hydration compounds produced and therefore, strength.
- Although previous studies have noted that a high SiO₂ content in the cement replacement would allow for an enhancement in strength with secondary hydration of Ca(OH)₂. This study noted that if parameters of the overall mix as shown in Equation 1 were taken into consideration, the increase in SiO₂ will have a negative impact on strength.
- When reviewing oxide values, oxide ratios provided the most accurate trendlines. Results showed when taking all parameters in consideration, the trend was like that of OPC hydration alone, in which Ca/Si determined the early age strength.
- Overall, results showed that the most accurate form of understanding the impact that chemical and physical variability of cementitious replacements would have, took into consideration both Ca/Si and the average particle size.
- ANN is a powerful tool in helping us gain a better understanding of the impact that each input has in relation to the target and allowing accurate prediction of the strength of concrete which incorporates cement replacements.
- ANN was successfully used in this study to provide an accurate prediction which correlated with the trends that were noted in the oxide analysis.



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Appendix A

| | | | | | |
|----|--------------------------|----|----------------------------|-----|------------------------|
| 1 | OPC20/PFA80* | 44 | OPC20.63/PFA68.12/SF11.25 | 87 | OPC5/GGBS60/BOS25 |
| 2 | PFA80/MK20 | 45 | OPC5/PFA80/SF15 | 88 | OPC30/GGBS40/BOS30 |
| 3 | OPC14/PFA56MK30 | 46 | OPC12.5/PFA80/SF7.5 | 89 | OPC35/GGBS20/BOS45 |
| 4 | OPC14/PFA66/MK20 | 47 | OPC60/PFA25/SF15 | 90 | OPC45/GGBS40/BOS15 |
| 5 | OPC24/PFA66/MK10 | 48 | OPC48.13/PFA48.12/SF7.5 | 91 | OPC45/GGBS20/BOS35 |
| 6 | OPC44/PFA26/MK30 | 49 | OPC60/PFA32.5/SF7.5 | 92 | OPC25/GGBS60/BOS15 |
| 7 | OPC60/PFA40 | 50 | OPC28.13/PFA68.12/SF3.75 | 93 | OPC15/GGBS40/BOS45 |
| 8 | OPC60/MK40 | 51 | OPC36.25/PFA56.25/SF7.5 | 94 | GGBS40/BOS60 |
| 9 | OPC27/PFA46/MK10 | 52 | OPC15/PFA80/SF5 | 95 | GGBS60/BOS40 |
| 10 | OPC28/PFA52/MK20 | 53 | OPC48.13/PFA40.62/SF11.25 | 96 | OPC47.5/PFA47.5/GP5 |
| 11 | OPC60/GGBS40 | 54 | OPC20.63/GGBS68.12/SF11.25 | 97 | OPC30/PFA50/GP20 |
| 12 | OPC14/GGBS56/MK30 | 55 | OPC5/GGBS80/SF15 | 98 | OPC27.5/PFA67.5/GP5 |
| 13 | OPC14/GGBS66/MK20 | 56 | OPC12.5/GGBS80/SF7.5 | 99 | OPC47.5/PFA37.5//GP15 |
| 14 | OPC44/GGBS46/MK10 | 57 | OPC60/GGBS25/SF15 | 100 | OPC35/PFA55/GP10 |
| 15 | OPC28/GGBS52/MK20 | 58 | OPC48.13/GGBS48.12/SF7.5 | 101 | OPC60/PFA20/GP20 |
| 16 | OPC24/GGBS66/MK10 | 59 | OPC60/GGBS32.5/SF7.5 | 102 | OPC10/PFA80/GP10 |
| 17 | OPC44/GGBS26/MK30 | 60 | OPC28.13/GGBS68.12/SF3.75 | 103 | OPC17.5/PFA67.5/GP15 |
| 18 | OPC20/GGBS80 | 61 | OPC36.25/GGBS56.25/SF7.5 | 104 | OPC60/PFA30/GP10 |
| 19 | OPC37.5/PFA57.5/BPD5 | 62 | OPC48.13/GGBS40.62/SF11.25 | 105 | OPC47.5/GGBS47.5/GP5 |
| 20 | OPC23.75/PFA68.75/BPD2.5 | 63 | OPC43/PFA38/GGBS19 | 106 | OPC30/GGBS50/GP20 |
| 21 | OPC28.75/PFA68.75/BPD25 | 64 | OPC24/PFA58/GGBS18 | 107 | OPC27.5/GGBS67.5/GP5 |
| 22 | OPC15/PFA80/BPD5 | 65 | OPC24/PFA18/GGBS58 | 108 | OPC47.5/GGBS37.5//GP15 |
| 23 | OPC60/PFA30/BPD10 | 66 | OPC14/PFA28/GGBS58 | 109 | OPC35/GGBS55/GP10 |
| 24 | OPC48.75/PFA48.75/BPD2.5 | 67 | OPC26/PFA37/GGBS37 | 110 | OPC40/GGBS60 |
| 25 | OPC60/PFA35/BPD5 | 68 | OPC14/PFA58/GGBS28 | 111 | OPC60/GGBS20/GP20 |
| 26 | OPC10/PFA80/BPD10 | 69 | OPC44/PFA18/GGBS38 | 112 | OPC10/GGBS80/GP10 |
| 27 | OPC48.75/PFA43.75/BPD7.5 | 70 | OPC5/PFA60/BOS25 | 113 | OPC17.5/GGBS67.5/GP15 |
| 28 | OPC37.5/GGBS57.5/BPD5 | 71 | OPC30/PFA40/BOS30 | 114 | OPC60/GGBS30/GP10 |



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| | | | | | |
|----|---------------------------|----|-------------------|-----|------------------|
| 29 | OPC23.75/GGBS68.75/BPD2.5 | 72 | OPC35/PFA20/BOS45 | 115 | OPC90/PFA-JUL10* |
| 30 | OPC28.75/GGBS68.75/BPD25 | 73 | OPC45/PFA40/BOS15 | 116 | OPC90/PFA-AUG10* |
| 31 | OPC15/GGBS80/BPD5 | 74 | OPC45/PFA20/BOS35 | 117 | OPC90/PFA-SEP10* |
| 32 | OPC60/GGBS30/BPD10 | 75 | OPC40/BOS60 | 118 | OPC90/PFA-OCT10* |
| 33 | OPC48.75/GGBS48.75/BPD2.5 | 76 | OPC25/PFA60/BOS15 | 119 | OPC90/PFA-NOV10* |
| 34 | OPC60/GGBS35/BPD5 | 77 | OPC15/PFA40/BOS45 | 120 | OPC90/PFA-DEC10* |
| 35 | OPC10/GGBS80/BPD10 | 78 | OPC60/BOS40 | 121 | OPC80/PFA-JUL20* |
| 36 | OPC48.75/GGBS43.75/BPD7.5 | 79 | OPC40/PFA60 | 122 | OPC80/PFA-AUG20* |
| 37 | OPC70/PFA-NOV30* | 80 | OPC90/BPD-JUL10* | 123 | OPC80/PFA-SEP20* |
| 38 | OPC70/PFA-DEC30* | 81 | OPC90/BPD-AUG10* | 124 | OPC80/PFA-OCT20* |
| 39 | OPC95/BPD-JUL5* | 82 | OPC90/BPD-SEP10* | 125 | OPC80/PFA-NOV20* |
| 40 | OPC95/BPD-AUG5* | 83 | OPC90/BPD-OCT10* | 126 | OPC80/PFA-DEC20* |
| 41 | OPC95/BPD-SEP5* | 84 | OPC90/BPD-NOV10* | 127 | OPC70/PFA-JUL30* |
| 42 | OPC95/BPD-OCT5* | 85 | OPC90/BPD-DEC10* | 128 | OPC70/PFA-AUG30* |
| 43 | OPC95/BPD-NOV5* | 86 | OPC95/BPD-DEC5* | 129 | OPC70/PFA-SEP30* |
| | | | | 130 | OPC70/PFA-OCT30* |

*OPC20/PFA80- 20%OPC and 80%PFA in the cementitious paste